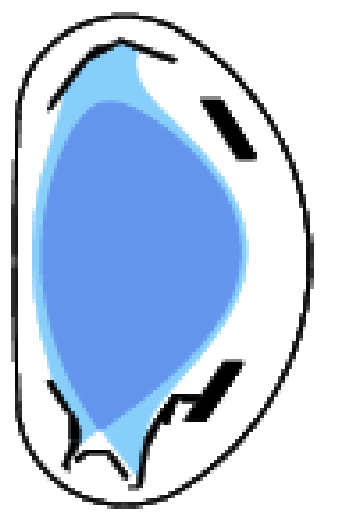


# Numerical optimization of ramp-down phases for TCV and AUG plasmas



ASDEX Upgrade

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MODEL

## 1. Research directions

**1. Development of an optimization procedure for the ramp down phase of the plasma discharge to terminate plasmas in the fastest and safest way:**

- Determination of **the optimal time evolution** of the plasma parameters, like **plasma current  $I_p$** , **plasma elongation  $\kappa$** , **auxiliary power  $P_{aux}$**  to terminate plasmas (decrease  $I_p$ ) as fast as possible.

- For safe termination **physical constraints** have to be specified: constraint on **normalized  $\beta_N$**  and **poloidal  $\beta_{pol}$**  (not too high) to avoid MHD modes, constraint on **plasma inductance  $L_i$**  to avoid vertical instability,...

- Define **technical constraints** to match experimental limits, like **max ramp rate of plasma current  $I_p$** , constraint on **rate of change in vertical magnetic field  $B_v$**  for radial position control,...

- Determination of optimal time of H- to L-mode transition.

**2. Development of the RAPTOR transport model:**

**The RAPTOR code** – Rapid Plasma Transport simulator [1,2]:

1D transport code without an equilibrium solver oriented to plasma real-time control.

- Time dependent geometry can be used.

- A new **gradient-based transport model** [3,4] for electron heat transport has been implemented.

- Successful validation via simulation of TCV and AUG full plasma discharges and comparison with the experimental measurements.

[1] F. Felici et al 2011 Nucl. Fusion **51** 083052

[2] F. Felici, O. Sauter 2012 PPCF **54** 025002

[3] O. Sauter et al 2014 Phys. of Plasma **21** 055906

[4] D. Kim et al 2016 PPCF **58** 055002

## 2. Trajectory optimization [2]

To get a good trajectory optimization

- 1) **realistic predictive simulations** ( $\Rightarrow$  an appropriate transport model) and
- 2) **fast solver** ( $\Rightarrow$  RAPTOR) are needed.

- Plasma current  $I_p$
- ECH power  $P_{ECH}$
- NBI power  $P_{NBI}$
- Plasma elongation  $\kappa$
- Poloidal flux  $\psi(p,t)$
- Electron temperature  $T_e(p,t)$
- Electron density  $n_e(p,t)$
- Ion temperature  $T_i(p,t)$

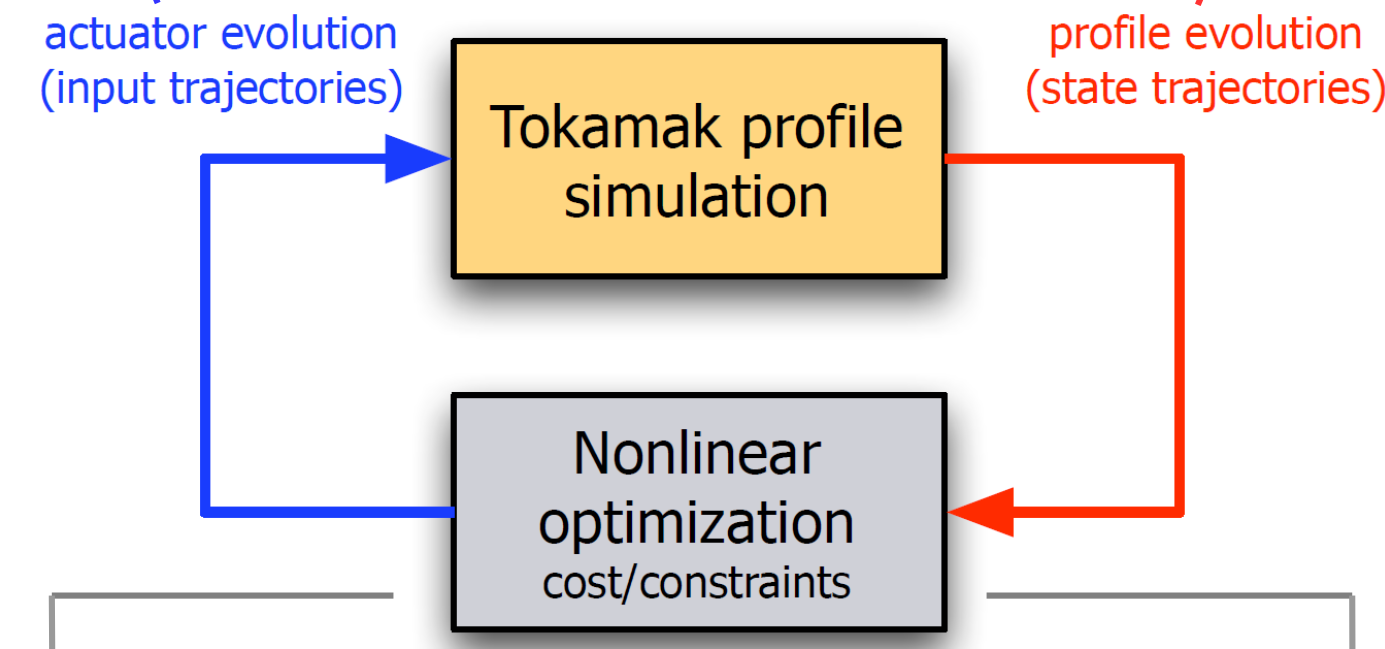


Fig. 1. Scheme of the nonlinear procedure for the actuator trajectories optimization [2].

**Cost function**

$$J = \sum_{i=1}^n v_i J_i; \min(J)$$

Examples:  $J_i = \|v_i(t_f) - v_{ref}\|_{W_i}^2$

$$J_{ss} = \|\partial U_p / \partial \rho\|_{W_{ss}}^2$$

$$J_{I_p} = \int I_p dt$$

**Constraints:**

- Safety factor  $q$  ( $>1.0$ )
- Plasma inductance  $L_i$  ( $>3$ )
- Edge loop voltage  $U_{pl}$
- ... various physical and technical constraints ( $I_p$  max ramp rate)

## 3. The transport model

**Diffusion equations:** electron temperature and poloidal flux

$$\frac{3}{2} (V')^{-5/3} \left( \frac{\partial}{\partial t} - \frac{\tilde{B}_0}{2 B_0} \frac{\partial}{\partial \rho} \right) \left[ (V')^{5/3} n_e T_e \right] = \frac{\partial}{\partial \rho} V' G_1 n_e \chi_e \frac{\partial T_e}{\partial \rho} + V' P_e$$

$$\sigma_1 \left( \frac{\partial \psi}{\partial t} - \frac{\rho \tilde{B}_0}{2 B_0} \frac{\partial \psi}{\partial \rho} \right) = \frac{J^2 R_0}{\mu_0 \rho} \frac{\partial}{\partial \rho} \left( \frac{G_2}{J} \frac{\partial \psi}{\partial \rho} \right) - \frac{V'}{2 \pi \rho} (j_{BS} + j_{CD})$$

**Electron heat diffusivity: gradient-based model [3,4]**

$$\chi_e = \frac{q_e}{V' \langle (\rho')^2 \rangle n_e T_e} \left[ \frac{\mu_{Te}}{T_e \rho_{edge}} f \left( \frac{\rho_{ped} - \rho}{\delta \rho_{ped}} \right) + \frac{\chi_{Te}}{\rho_{edge}} f \left( \frac{\rho - \rho_{ped}}{\delta \rho_{ped}} \right) \right]^{-1} \times f \left( \frac{\rho_{inv} - \rho}{\delta \rho_{inv}} \right) + \chi_{ST} f \left( \frac{\rho - \rho_{inv}}{\delta \rho_{inv}} \right)$$

$\chi_{Te}$  – fixed parameter for L- and H-modes  
3.2 for TCV L-mode, 3.0/2.3 for AUG L-/H-mode.

or controlled parameter to get a given  $H_e$

$$\mu_{Te} = \left( \frac{H_e \tau_{scf}}{\tau_{Ee}} \right)_{time}$$

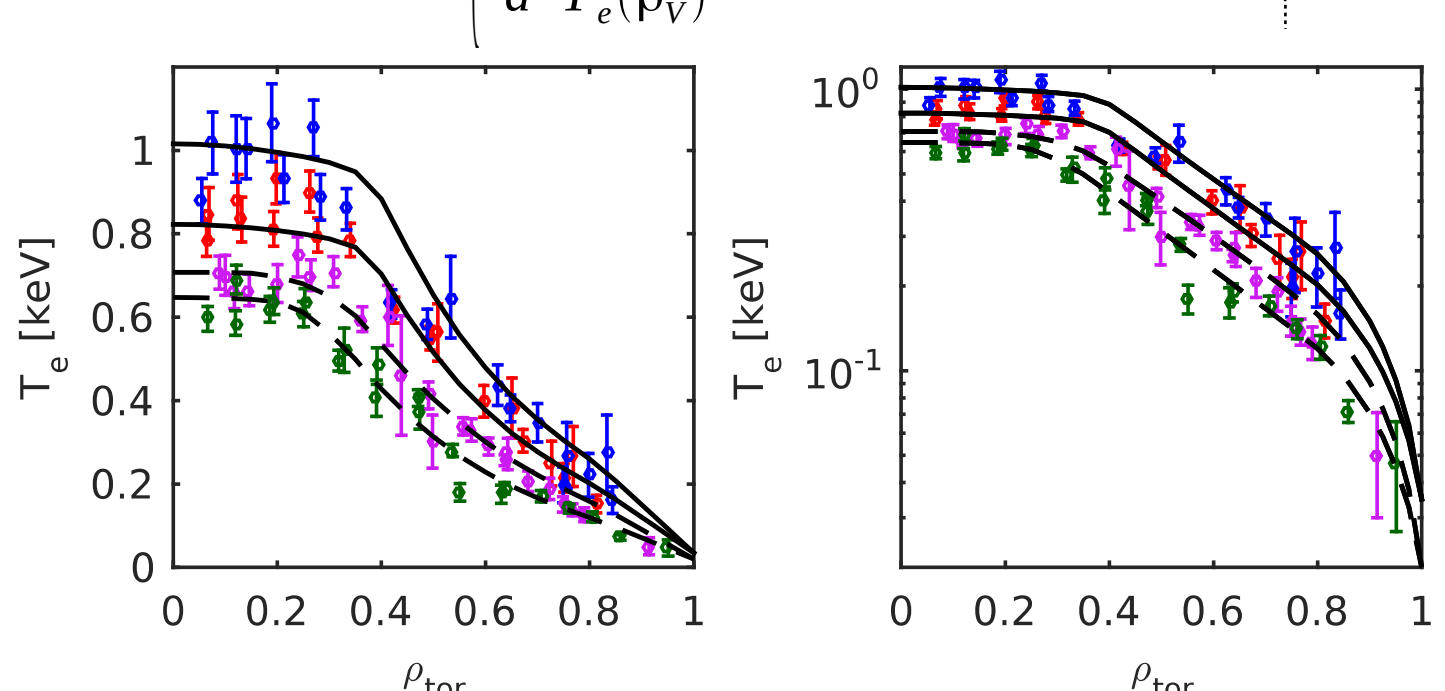


Fig. 2. RAPTOR simulated profiles (black solid) vs the experimental ones for the TCV shots: #50719  $I_p=195$  kA, #50719  $I_p=206$  kA, #53851  $I_p=205$  kA, #53851  $I_p=185$  kA.

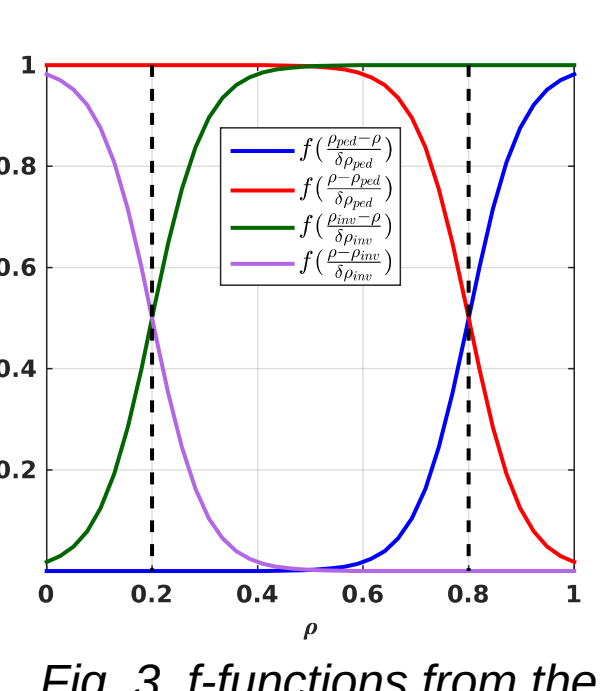
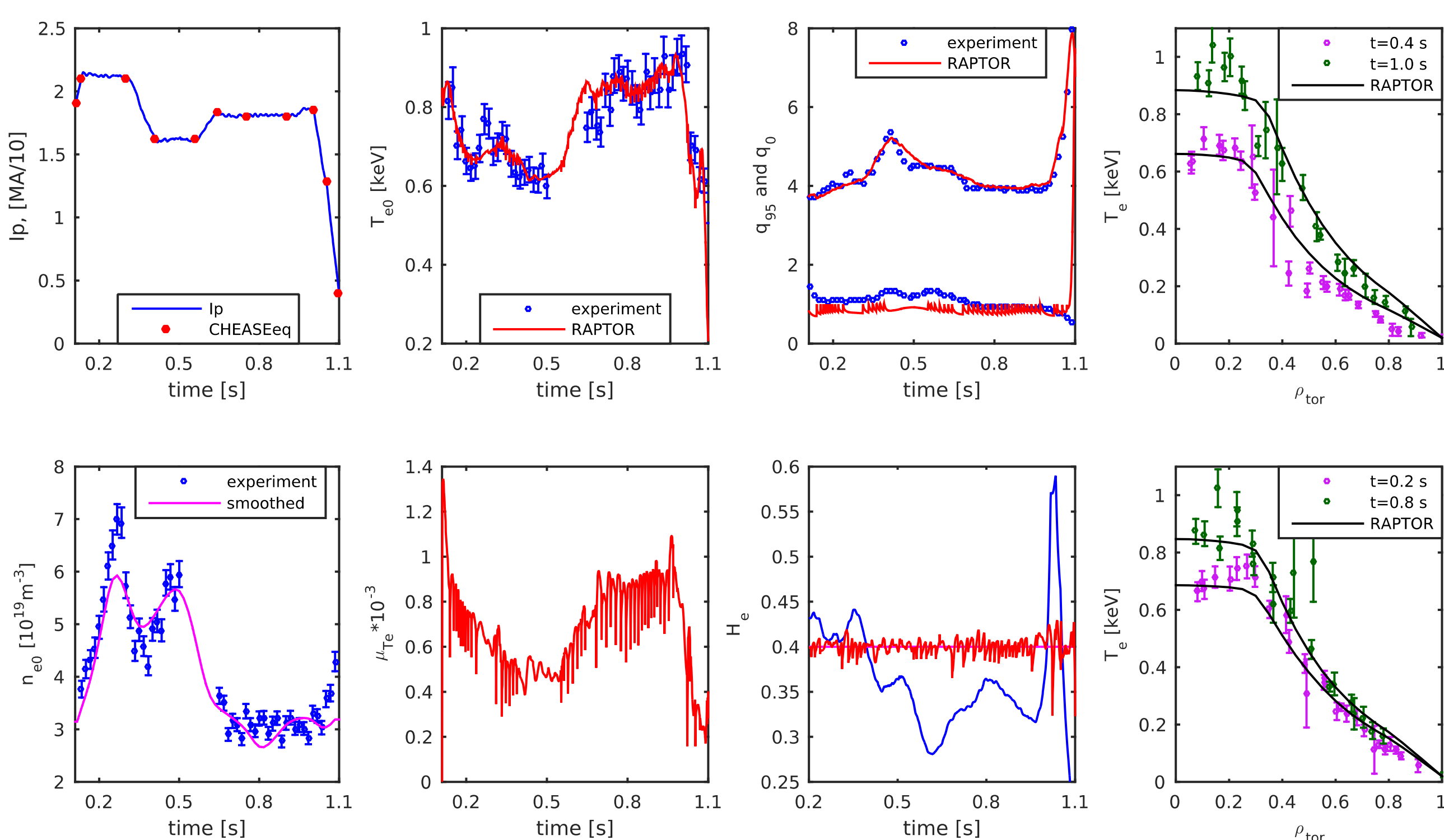


Fig. 3. f-functions from the formula for  $\chi_e$ .

VALIDATION

## 4. Full TCV plasma simulation: #53852, ohmic plasma, L-mode



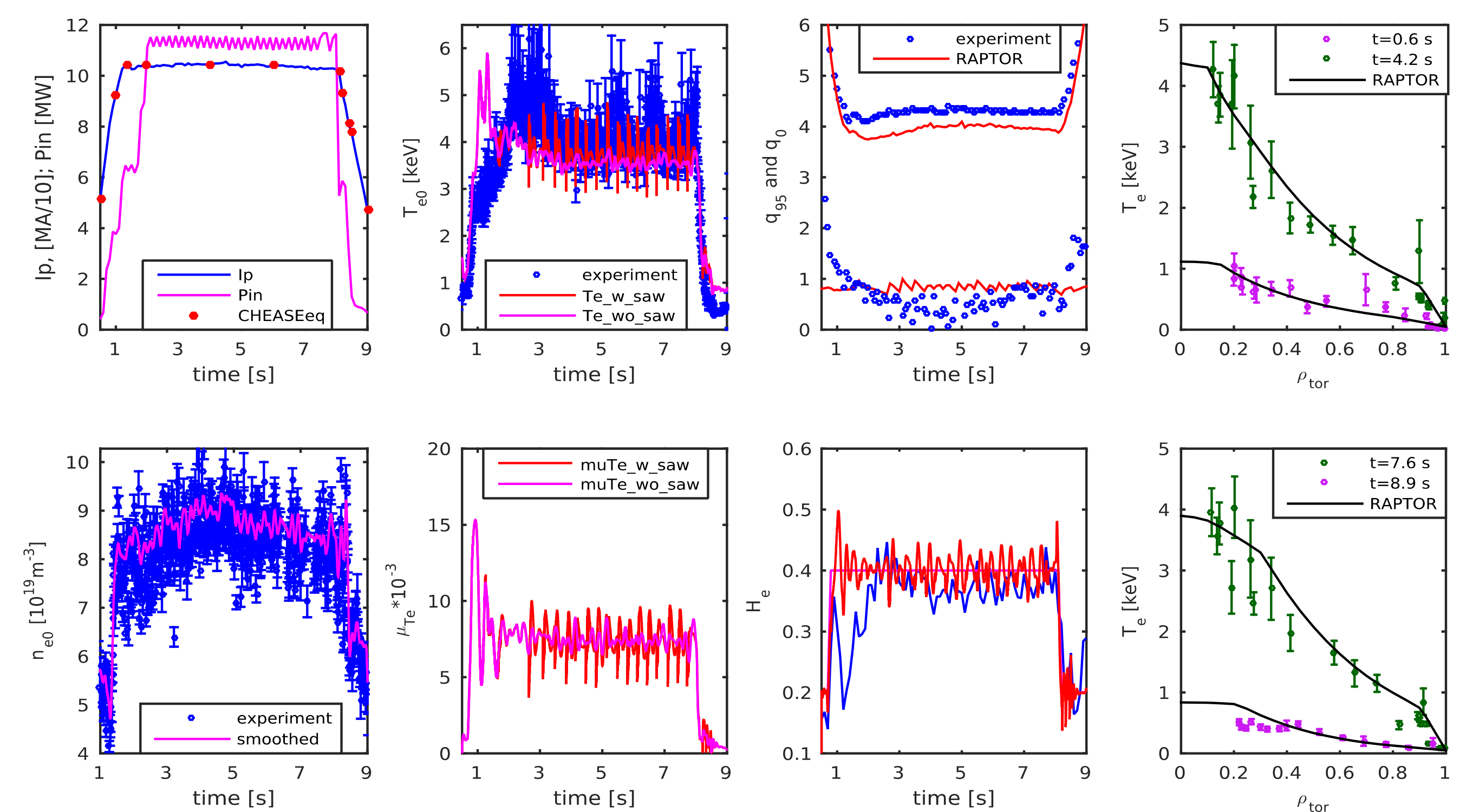
**Prescribed parameters:** total plasma current  $I_p$  over time, radial profiles of electron density  $n_e$  over time,  $H_e$  factor fixed at 0.4,  $\lambda_{Te}=3.2$  ( $\lambda_{Te}$  line averaged electron density  $n_{el}$  if  $n_e(p,t)$  not provided), scaling law H98(y,2) for total confinement time.

**Predicted variables:** electron temperature  $T_e$ , poloidal flux  $\psi$ , electron heat diffusivity  $\chi_e$ , various physical quantities.

**Equilibrium:** 10 CHEASE equilibria (marked as  $\bullet$  on the  $I_p$  plot).

**CPU time:** less than 2 min for a time grid with 1 ms step (shot duration 1 s) on a standard PC.

## 5. Full AUG plasma simulation: #32546, NBH, ECRH, L-H-L modes



**Prescribed parameters:** same as for TCV case, total input NBI and EC power over time and their deposition,  $H_e$  factor fixed at 0.4 for H-mode and at 0.2 for L-mode,  $\lambda_{Te}=3.0/2.3$  for L-/H-mode, Gaussian radial profiles for heating sources.

**Predicted variables:** as for TCV case

**Equilibrium:** 11 CHEASE equilibria (marked as  $\bullet$  on the  $I_p$  plot).

**CPU time:** less than 10 min for a time grid with 1 ms step (shot duration 8.5 s) on a standard PC.

OPTIMIZATION

## 6. Generic ramp down optimization

**Ramp down optimization of plasma current and elongation at  $t=0.5$  s for AUG-like plasma:** cost function  $J_{I_p} = \int I_p dt$

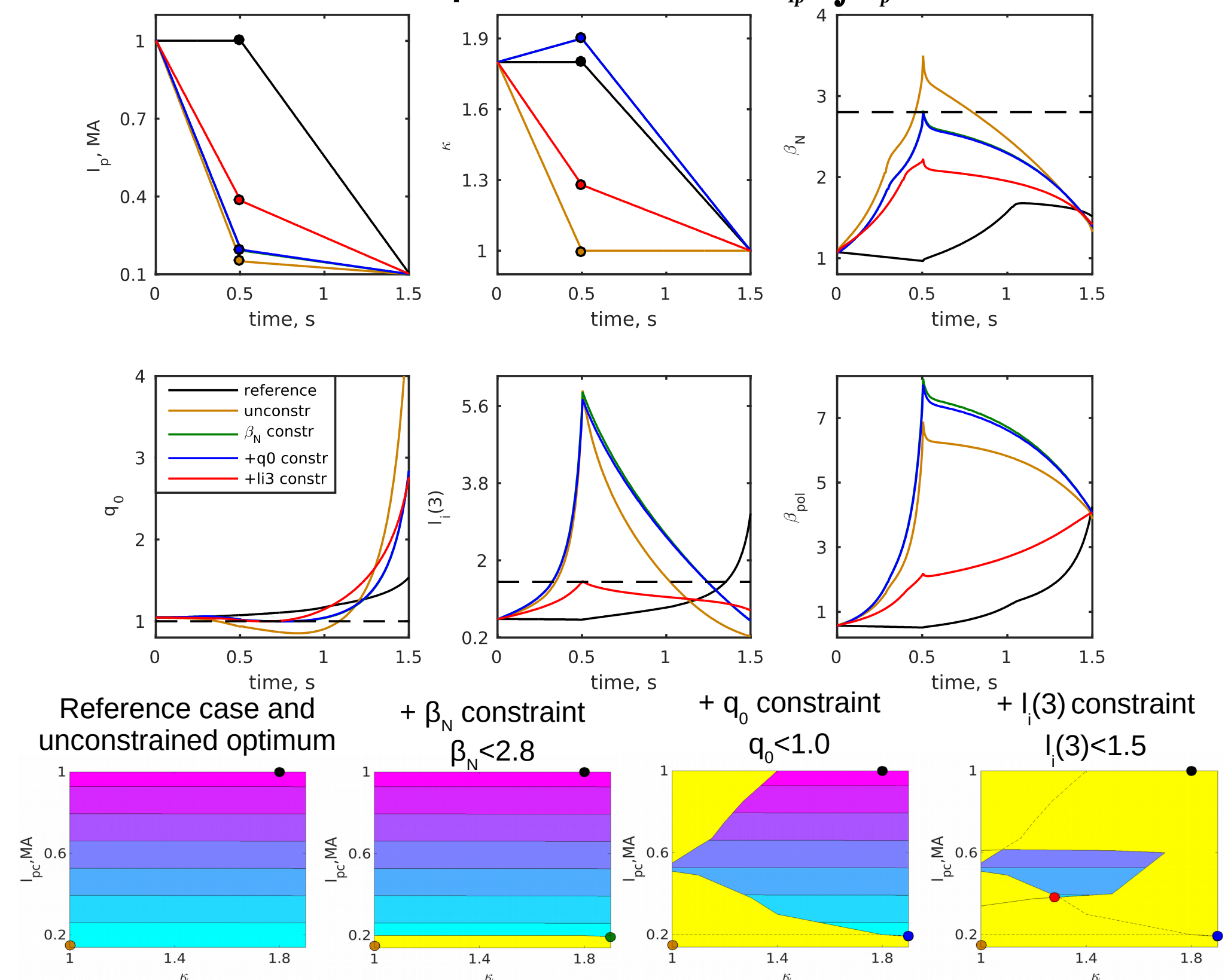
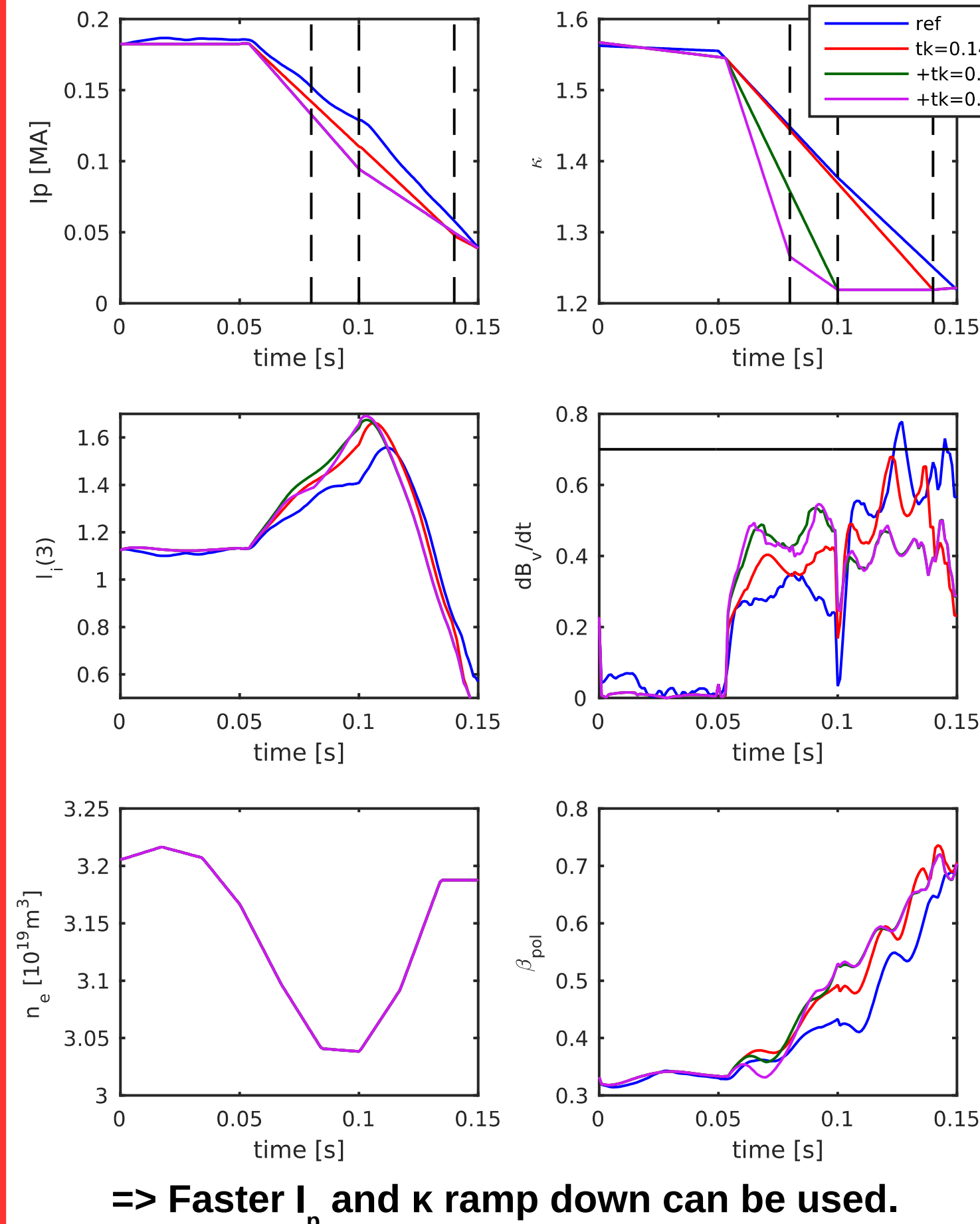


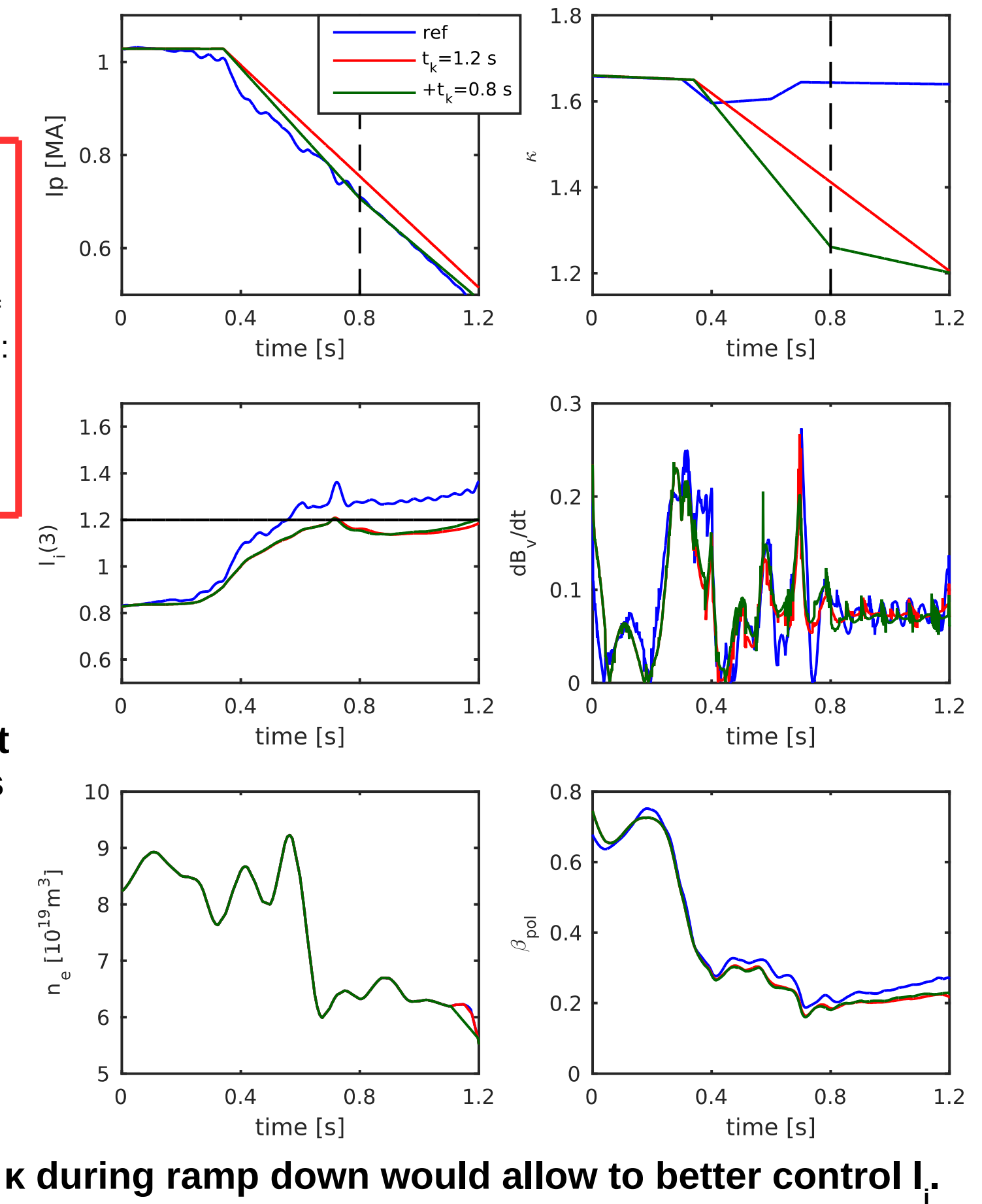
Fig. 4. The contours for  $J_{I_p}$  are shown with the coloured circles which correspond to values of  $I_p$  and  $\kappa$  at  $t=0.5$  s. An area where the constrained parameter violates the constraint is yellow-marked.

## 7. Ramp-down optimization: TCV #53852



$\Rightarrow$  Faster  $I_p$  and  $\kappa$  ramp down can be used.

## 8. Ramp-down optimization: AUG #32546



$\Rightarrow$  Reducing  $\kappa$  during ramp down would allow to better control  $I_p$ .

PLANS

## 9. Further research directions

**1. Need better control on  $\mu_{Te}$  (less oscillations):**

now  $\mu_{Te}$  = feed-forward + feed-back control.

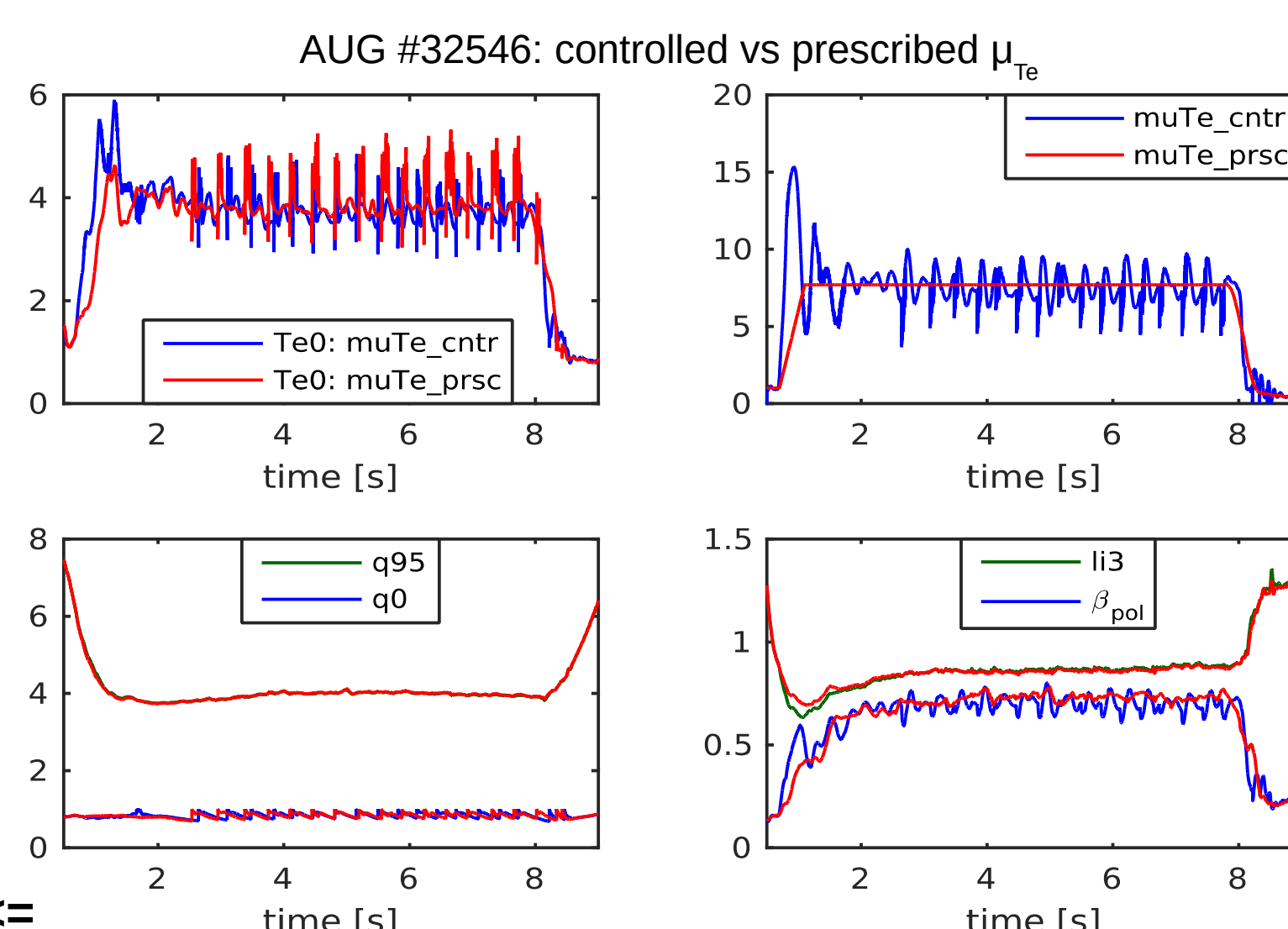
$$\mu_{Te} = \underbrace{\mu_{Te}^{ff}}_{\text{feed-forward}} + \underbrace{K_p \cdot err(t) + K_i \cdot \int err(t) dt}_{\text{feed-back}}$$

where  $err(t) = H_e^{ref} - H_e^{calc} = H_e^{ref} - \tau_{Ee} / \tau_{scf}$

Feed-forward law for  $\mu_{Te}$  via relation with  $T_e(p_{ped})$ :

$$\mu_{Te}^{ff} = - \frac{dT_e}{d\rho} = - \frac{T_e(p_{ped}) - T_e^{BC}}{\rho_{ped} - 1.0}$$

Present oscillations do not disturb physics result  $\Leftarrow$



now  $T_e(p_{ped})$  for  $\mu_{Te}^{ff}$  is estimated:  $T_e(p_{ped}) = T_{e0} \exp(-\lambda_{Te}(\rho_{ped} - \rho_{inv}))$

$T_{e0}$  scaling law for TCV:  $T_{e0} = 7.5 \cdot 10^3 \cdot (I_p [MA])^{0.93} \cdot (P_{tot} [MW])^{0.3} \cdot (n_e [10^{19} m^{-3}])^{-0.6}$

$T_{e0}$  scaling law for AUG:  $T_{e0} = 3.3 \cdot 10^3 \cdot (I_p [MA])^{0.93} \cdot (P_{tot} [MW])^{0.3} \cdot (n_e [10^{19} m^{-3}])^{-0.6}$

**2. Need a scaling law for pedestal pressure for L-/H-mode (to determine  $\mu_{Te}$  directly).**

**3. Include diffusion equation for electron density to the transport model:**

now prescribed  $n_e$  is used;

now to keep density within Greenwald density limit during optimization:  $n_e(0,t) = \min(n_{ref}(0,t), n_{GR}) = \min(n_{ref}(0,t), 0.9 \frac{I_p(t)}{\pi a^2})$

**4. Continue ramp-down optimization with an extended set of parameters:**

- time of H- to L-mode transition as an optimization parameter (already implemented, need tests);
- constraints related to radiated power and impurities;
- technical constraints on rate of change of electron density, plasma shape;
- technical constraint on vertical position control (constraint on  $dl/dt$ ).

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